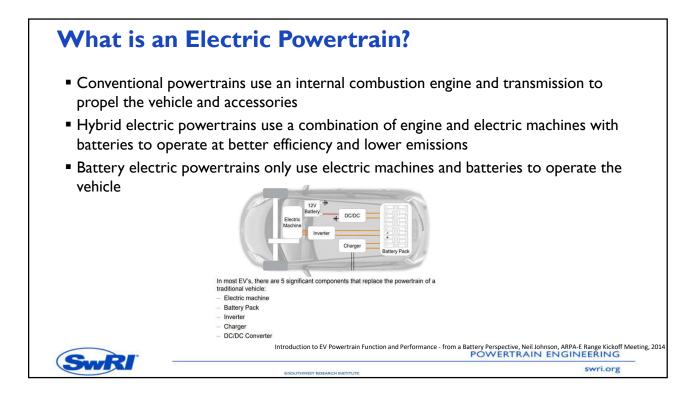


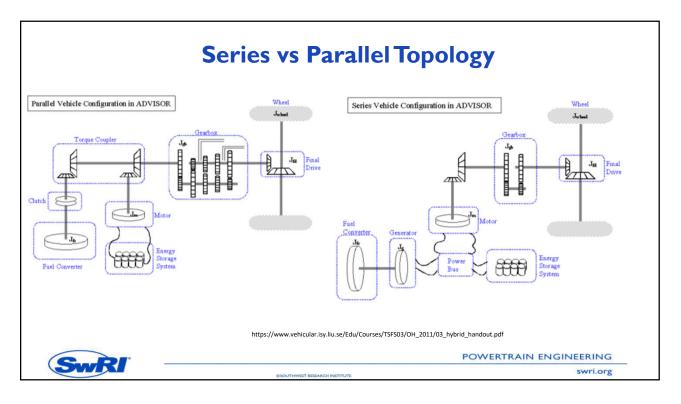
# Introduction to Electric Powertrains

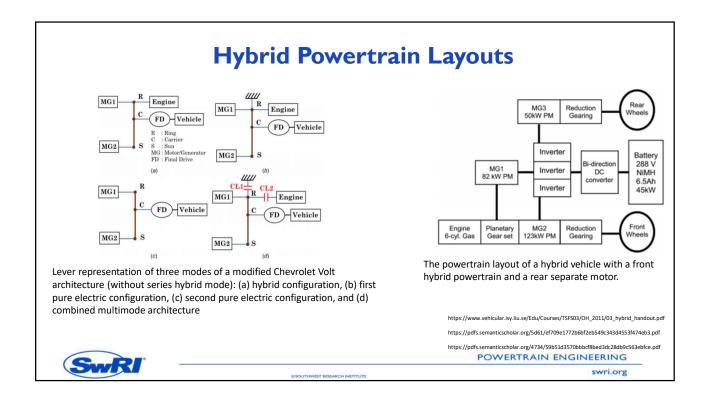
# **State of Industry**

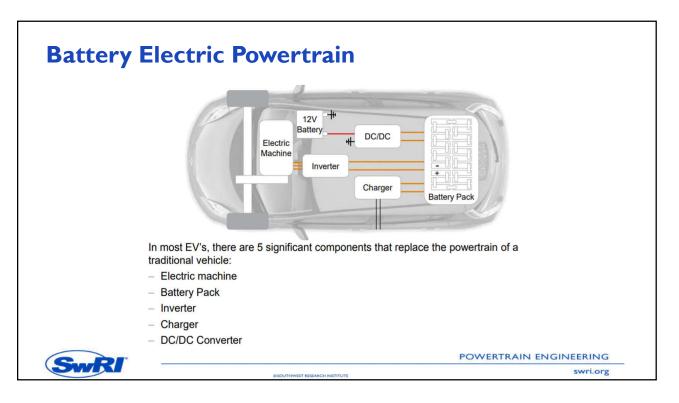
- On road light and heavy duty electrification is an irreversible trend to achieve lower emissions and better fuel economy
  - Strong synergies with performance, comfort and autonomous driving
- Off road electrification is being driven by productivity and logistics
- Mining industry has initiated electrification efforts primarily for the lower vehicle emissions and the prospect of reducing air handling costs
- While cost limits rate of electrification growth in other industries, mining industry can realize overall cost reduction
- Energy recovery capabilities also limit heat generation from the powertrain

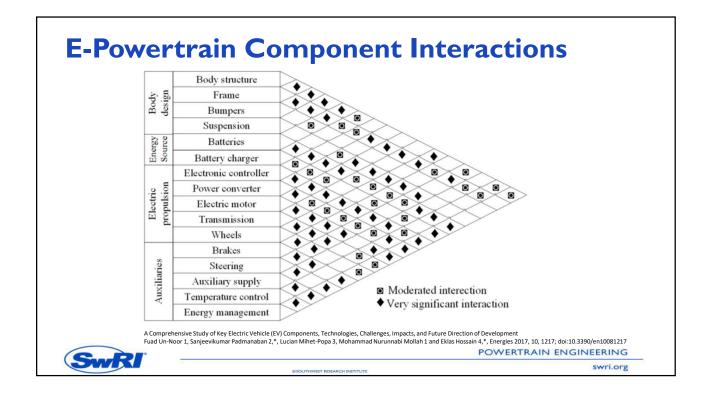


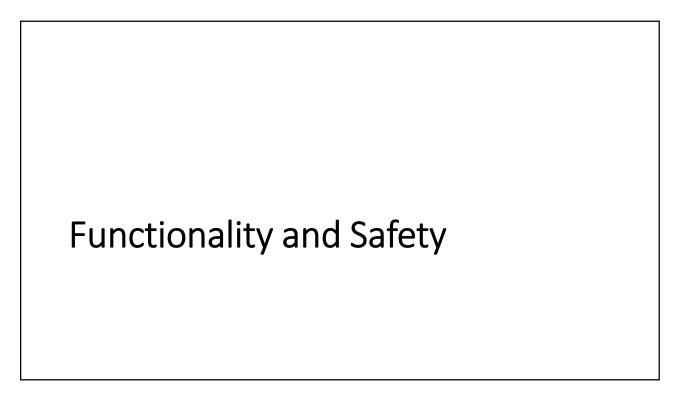


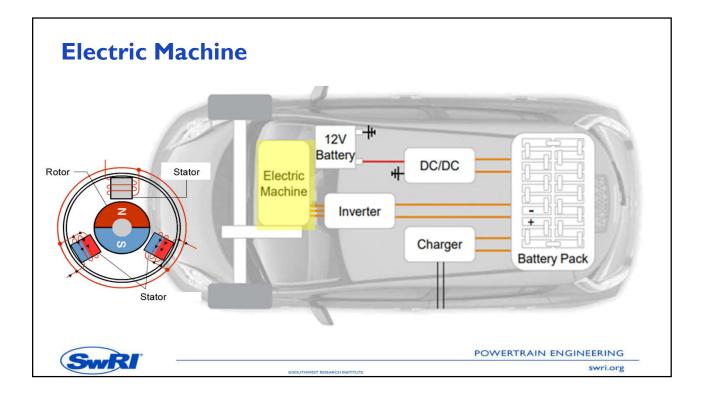


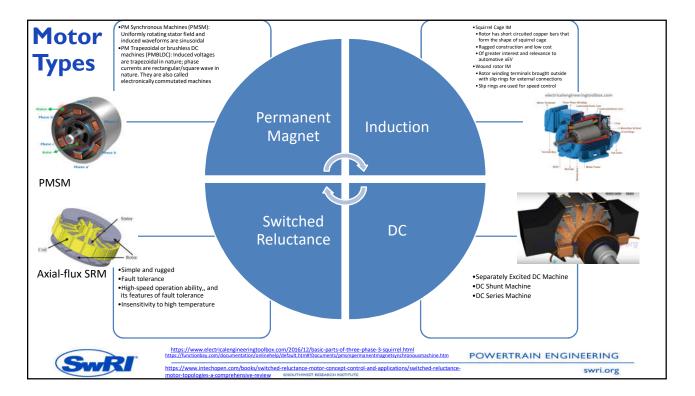


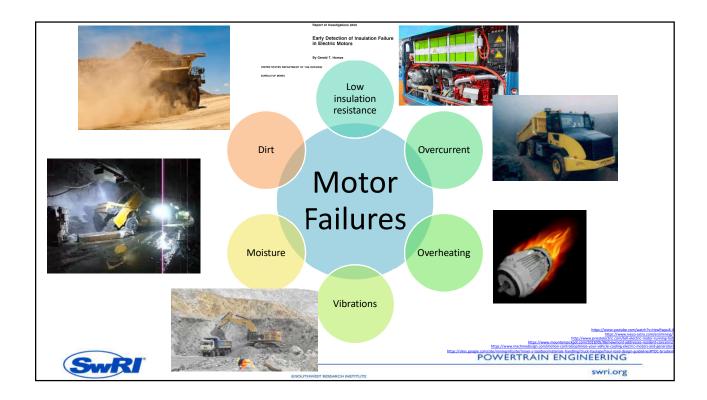










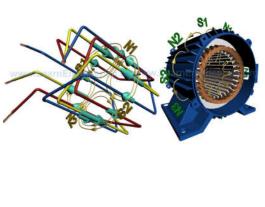


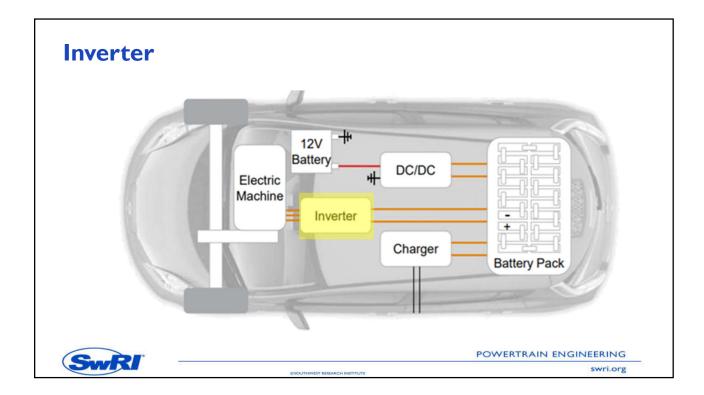
# **Balance of Magnetic Fields in Rotor**

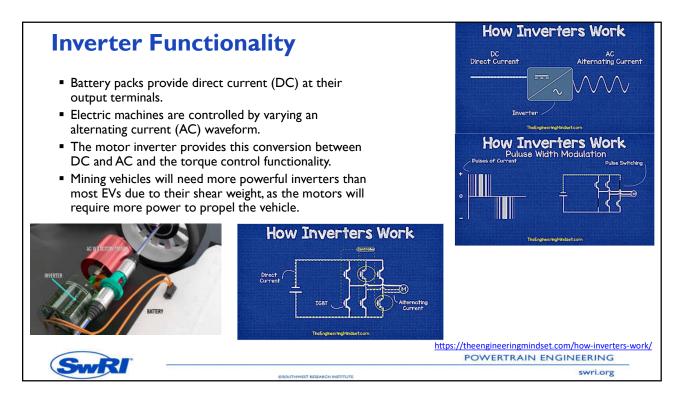
- Like the tires on a car, having a balanced rotor and uniform intensity rotor levitation magnets will make for a smooth running motor. Since there is so little friction with the rotor levitated, the least bit of out of balance or non-uniform magnet strength shows up. Most rotors are going to be a little bit out of balance. The slightest out of balance of the rotor will cause the rotor to bounce around at some rotation speeds similar to car tires. Some speeds are much worse than others. I've noticed that the major out of balance oscillations of my motor are over a rather small range at low rpm. There seems to be another out of balanced condition at very high speeds.
- When running the motor on low voltages, the bouncing around affect of the free end of the rotor can cause the motor to not be able to speed up above the out of balance speed. The bouncing around of the rotor can cause the rotor to fly off the levitation field. When this happens the rotor will crash onto the stator magnets.

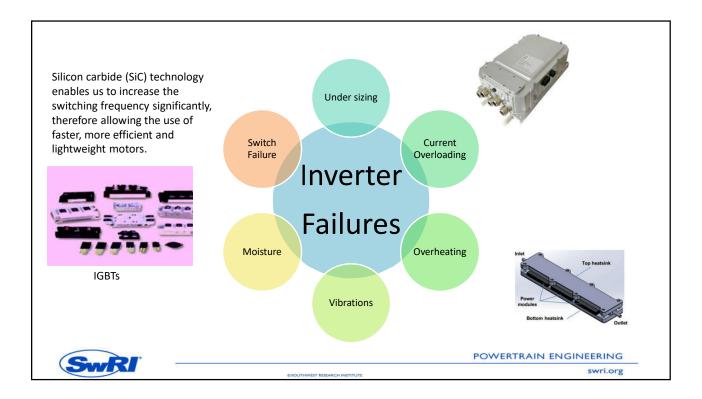
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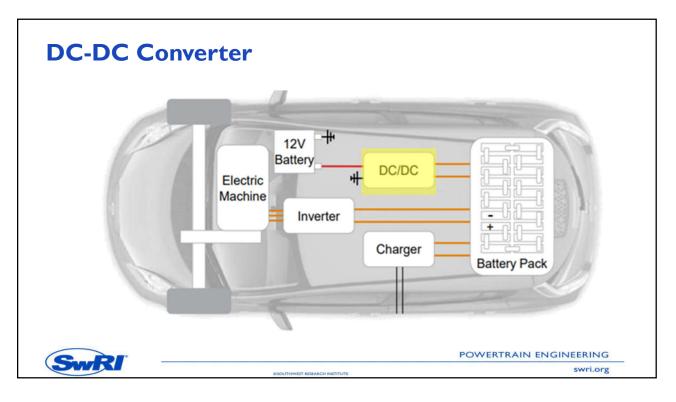
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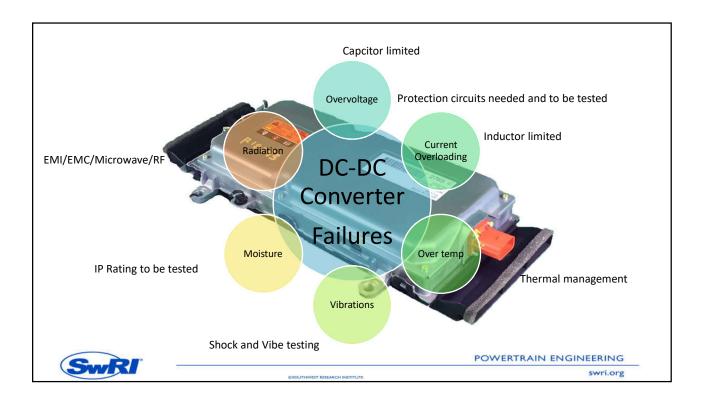


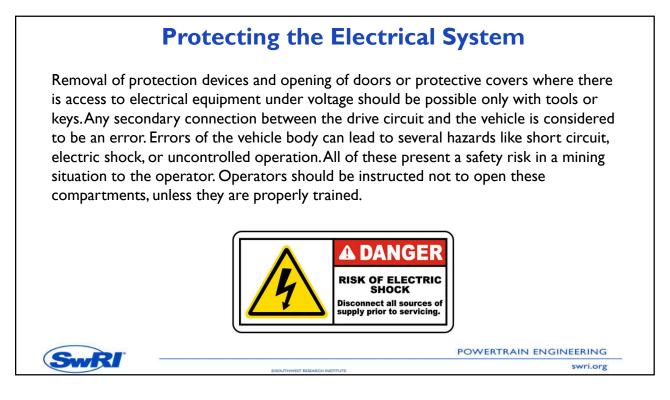


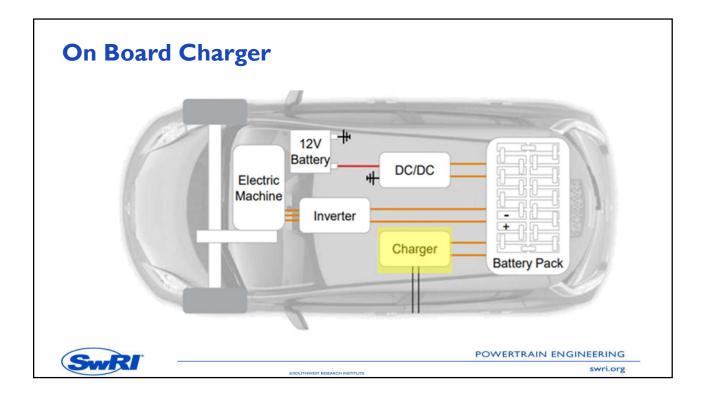


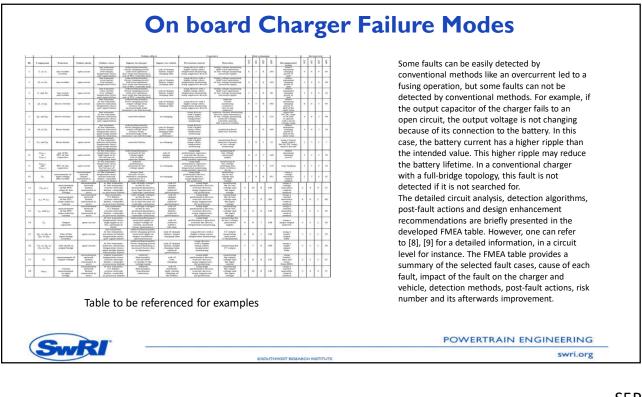










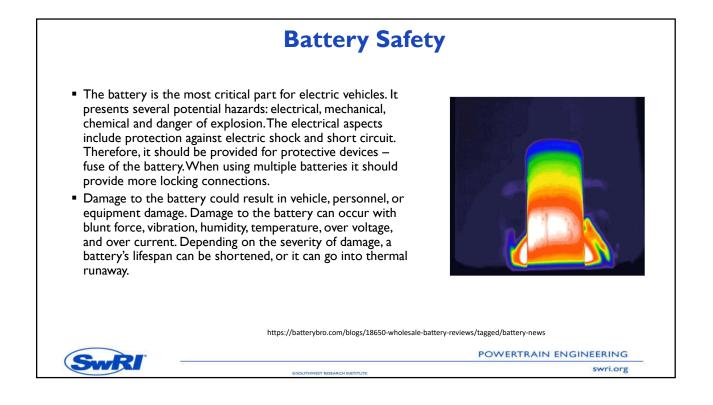


# **On Board Charger Failure Modes**

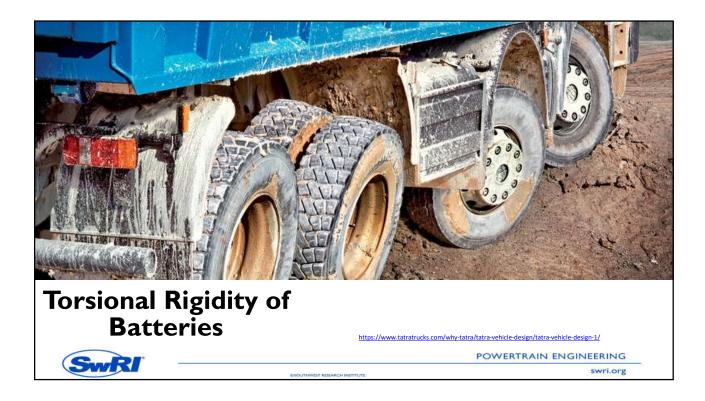
- In the component field of the table, it is stated which component or combination of components have a failure. In the next field of the table, failure mode, the device status after failure is explained. For instance, if one or more diodes are failed, it can lead an open circuit or a short circuit status. The failure causes, are the main roots of the failure that have direct correlation with the occurrence number.
- Failure effects are the next part of the table that shows how one particular case affects the charger and vehicle. This part has direct relation with severity. Prevention control and detection methods are the next fields in the table that show how one can reduce those failures. The risk evaluation is the next part in which risk priority numbers are provided as the result. If one fault is occurred, there are recommended action(s) to enhance the performance or equivalently to reduce RPN for each case, if it is possible. In most of cases, the RPM numbers are reduced after proposed post-fault actions that is equivalent to an increased reliability. As the next step of this work, one can calculate the reliability of the charger to see in a quantitative manner how much reliability improvement is achieved. This table can expanded to cover more faults like the semiconductors failure to an open circuit status.

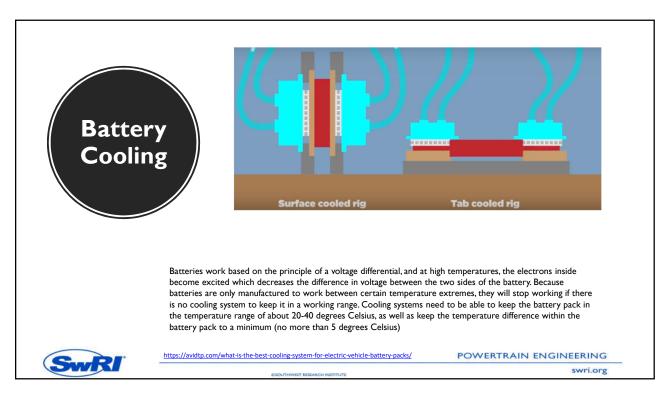
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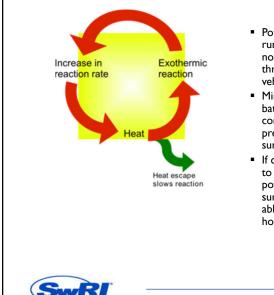
Electric Machine Inverter Charger Battery Pack	rter Charger
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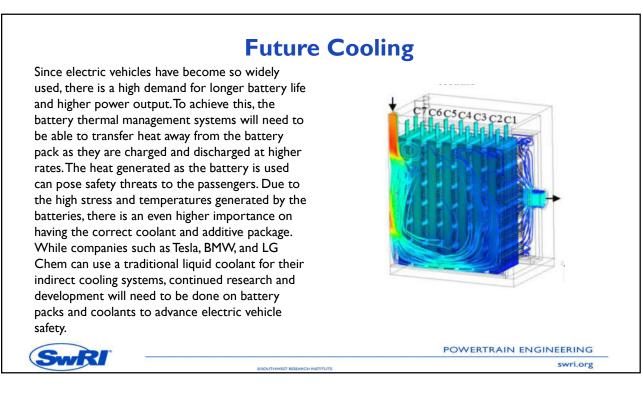




# Failure to Cool a Battery

- Potential thermal stability issues, such as capacity degradation, thermal runaway, and fire explosion, could occur if the battery overheats or if there is non-uniform temperature distribution in the battery pack. In the face of lifethreatening safety issues, innovation is continually happening in the electric vehicle industry to improve battery cooling systems.
- Mining Vehicles require large battery coolers, as they tend to have large batteries. These cooling systems need to be designed in spec with mining conditions, as to not break. If the cooling system works through liquid, precautions need to be taken so that the system is well protected from its surrounding, as to not spill large amounts of coolant over the mine.
- If cooling system does fail, the vehicle should not be allowed to send power to the wheels any longer. If on an incline, battery power should go solely to powering the brake booster and allowing the vehicle to lower itself to a flat surface if possible. Once the vehicle is on a flat surface, or vehicle is safely able to be towed, a recovery vehicle should retrieve it and bring it back to home for analysis.

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# Heating the Battery

Substantial range reductions in the cold. Mining operations taking place in cold climates will need to take precautions.
Regenerative braking is severely reduced because the battery

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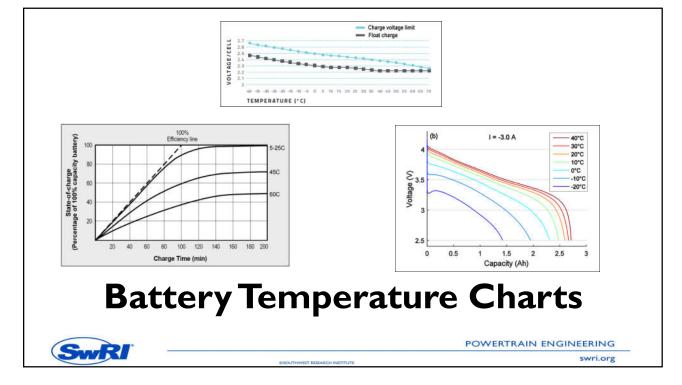
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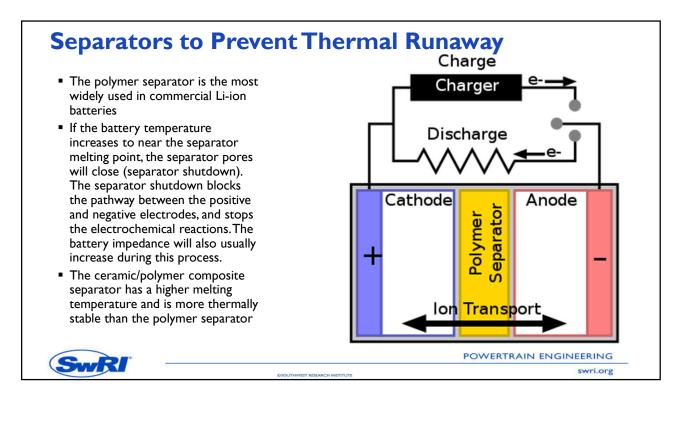
cannot take in the rate of charge energy from braking

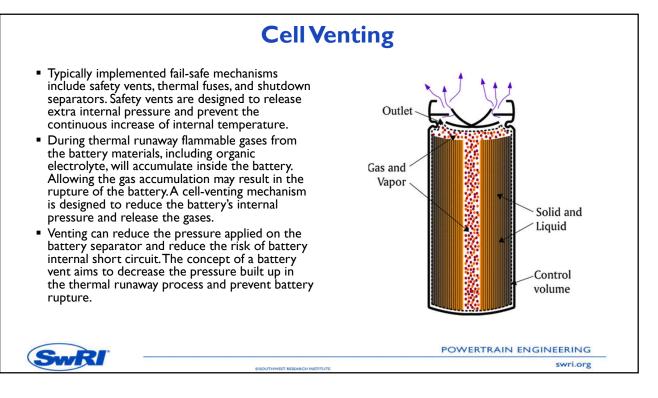
Lithium Battery for Cold Weather Applications | RELION, Sep 2018 Tesla Model 3 — Cold Weather Tips – Tom Harrison's Blog, Dec 2018

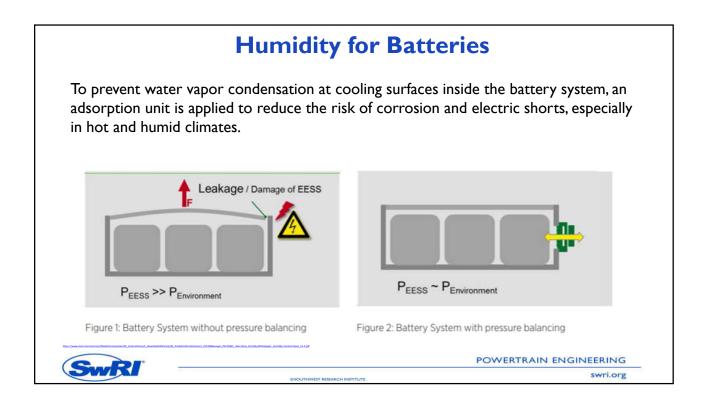


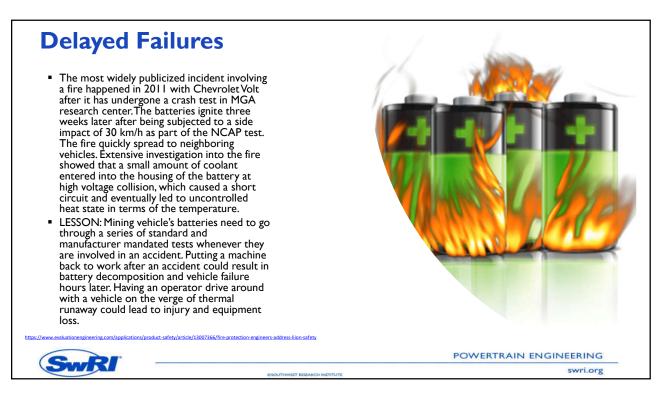
Lithium plating issues







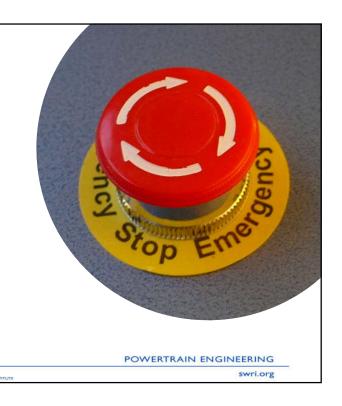




# Switch In Case of a Crash

- Risks from an accident include potential electric shock from damaged systems that are turned off during or immediately after crash. Because of this, the association recommends that manufacturers of electrical vehicles install switches that will stop the energy from the battery case in accident. The location of these switches must be standardized for security. Drivers of towing services also need to be well informed and trained on how to deal with hybrid and electric vehicles. The danger can be reduced if people from emergency services have easy access to batteries and if vehicle manufacturers create unique location for exclusion to all electric and hybrid vehicles.
- Pathways and routes should be planned so that tow vehicles have access to a damaged EV.All killswitches should be able to be activated no matter what position the vehicle is it.







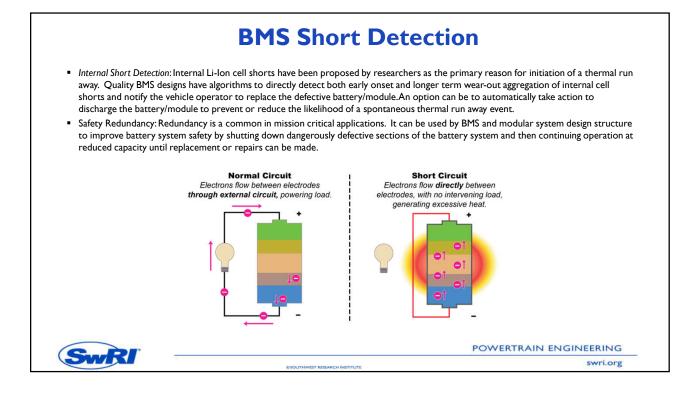
# Working with batteries

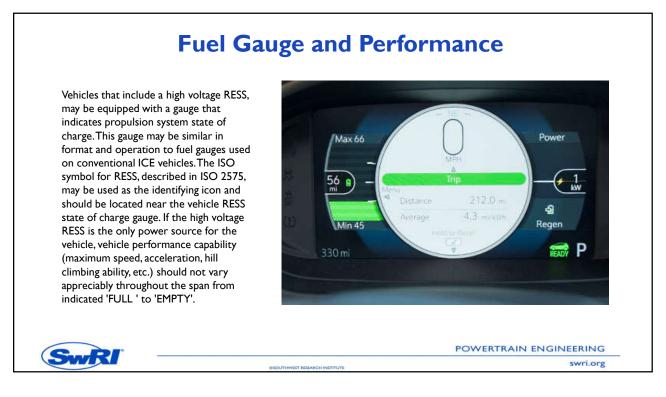
 On the Mining Safety portal we have emphasized the importance of wearing personal protective equipment. This requirement also extends to those working in the battery charging room. The Personal protective equipment (PPE) required when working with batteries includes: Approved face shield and goggles Approved acid-resistive gloves with gauntlets of at least 6 to 8 inches Approved full-length rubber apron Slip- and acid-resistive footwear with protected toe Nonconductive tools, including scrapers, mops and brushes Adequate number of ABC re extinguishers that are properly inspected/maintained Adequate amount of neutralizer Workers should protect open cuts or lesions with plastic patches. They should also refrain from carrying batteries by their terminal posts and always use an appropriate strap

https://www.miningsafety.co.za/dynamiccontent/125/battery-charging-rooms-and-mining-safety SwR

ignition sources permitted.

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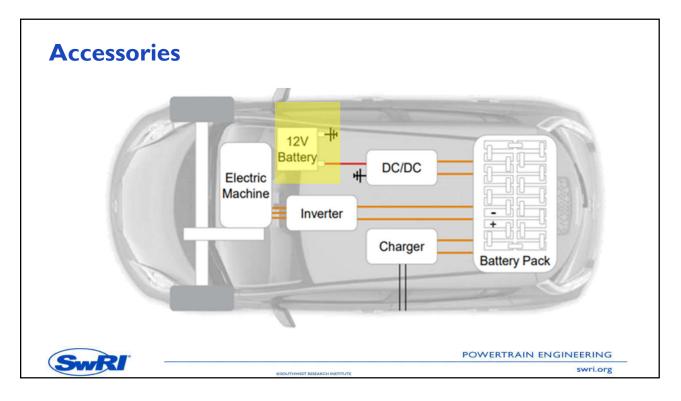


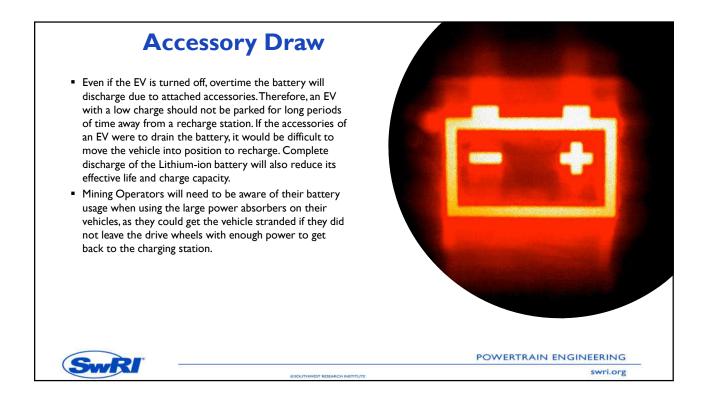
#### MDEC 2019

### Fuel Gauge and Performance cont.

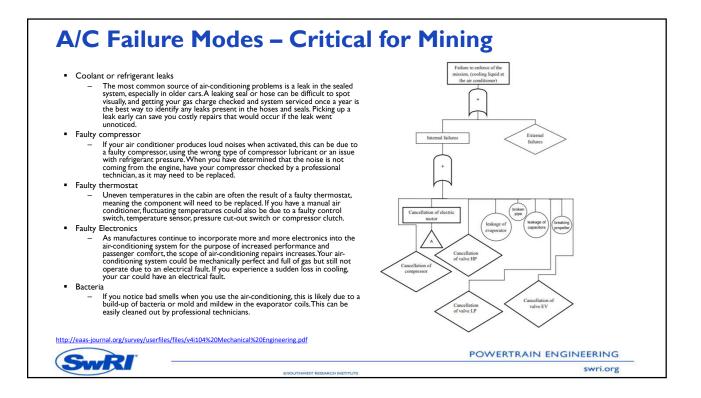
If the vehicle is designed to provide a reduced level of performance as the high voltage RESS state-of-charge becomes depleted (to protect RESS life, provide a "limp home" feature, etc.), a separate indicator shall be activated to alert the driver when this reduced level of performance is invoked. This indicator and its corresponding reduced level of vehicle performance should be explained in the owner's manual. In case that the high voltage RESS is the only power source of the vehicle, whenever there is sufficient RESS state-of charge to propel the vehicle, including all normal and reduced performance operating modes, there shall be no discernible degradation in the performance of critical vehicle safety systems such as lighting, braking, steering, etc.

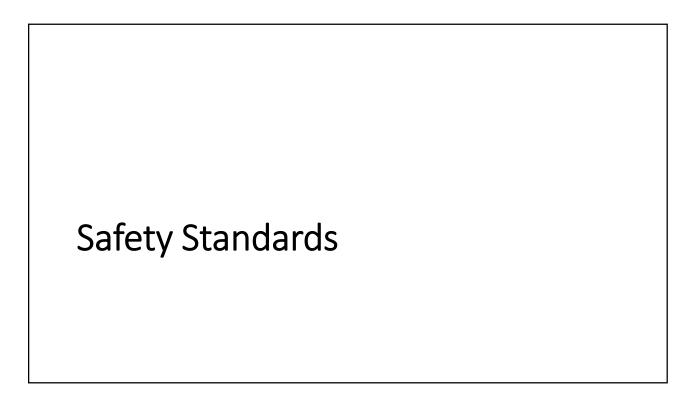


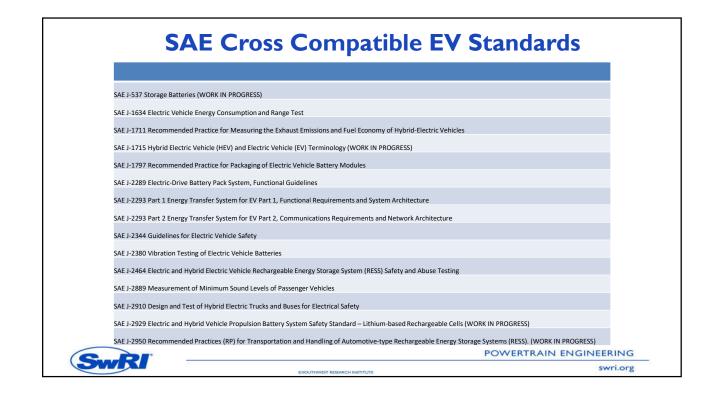




CAUSE OVERVOLTAGE	FAILURE PHENOMENA	CONSEQUENCE	REMARKS	
Exceeding the maxi-		Short fame (self-extinguished), a		PTC Heater Failure Mode
mam rated voltage or	greater then the heat which can be	burn hole, mellod soldered joint,	ranging from microseconds to milli-	
the minimum hold vol-	dissipated. The temperature of the	detached leads failing out of the	seconds will not provoke any failure	
tage by at least 25 %.		ceramic. Depending on available power a short circuit is also possi-	of this type as the energy is too low to	
	corresponding to the resistance maximum. The material enters a	power a short circuit is also poss-	heal the PTC above its maximum resistance.	
	NTC zone with a thermal runway		Deservices on the thermal senarity of	
	the state war a contractional		the ceramic, overvotage of short	
			durations (- 1 s to 10 s) will not pro-	
			sole talure.	
OVERCURRENT DENSIT		Durned electrode, small scarks,		
		Durned electrode, small sparka, eventual flashover, positive resis-	In practice, this current is hardly ever reached, as the ceramic bulk resis-	
metalization layer.	The contact can be a combination	tance shill	tance is sufficient to restrict unac-	PTC air heater
	of lead-solder, metallization layer		ceptable increases. Only in special	FTC air neater
	or clamping contact and metalliza-		cases, such as votage spikes with	Index of the second s
	Son layer.		high energy (+ 100 A) can this current	
	- Ni	1	be exceeded.	
OVERPOWER				
		In both cases, there will be ceramic		
			PTC can have is also influenced by the way he is attached to the electri-	
	duce thermal gradients as high as 1500 "Cicm. This gradient will pro-		cal contacts, Large thermal masses	
current and voltage	voke mechanical shain due to	Fails open.	on the electrodes reduce the maxi-	
which are not guaran-	thermal expansion mismatches.	For high voltage types (> 400 V) a	mum power a ceramic can sustain.	
leed by the manufac-	Two different phenomena can	possible local hot-spot can drive the		
turer.		cerumic into thermal runway. This		
		special condition can generate the		
		same consequences as described		
	insah currenta, when the power per mm3 is exceeded. Overpower	in Overvoltage'.		
	per mills is exceeded. Overpower shree the awhith temperature			
	occurs when a combination of final			
	voltage and maximum current du-			
	ring switching is exceeded.			
THERMAL SHOCK				
Caused by an uneven			When thermal shock is caused by	
power distribution within	is not evenly divided over the	breaking up of the ceramic can be a	micro-cracka, the cracking-up or	
			breaking of the ceramic is not always	
searing from the los-	some parts will heat up faster than others (the centre heating up the	micro-cocks every line they are	visce on the surface.	
region.	fastest). These temperature gradi-	Fails open.		
241422	ents will provoke expansion mis-	and a state of the		
BEDUCTION EFFECT	nath		L	
	An unstable material surrounding	See 'Devotion'		
bie material (such as:	or even touching the ceramic will			
wax, poting material,	typically disintegrate or burn at			
glue, lacquer, thermal	high temperatures. This is an ory-			
steeves, appressive	gen consuming phenomenon.			
(washing) fluids and	When in close contact with the			
	PTC, the material may react with oxygen of the grain boundaries,			
In cose contact with	brygen of the grain boundaries, thus reducing the PTC caramic			
	and in turn its maximum rated volt-			
	age or hold voltage.			
NUMBER OF CYCLES		-		
Repetitive tripping of	Repetitive cycling introduces	Leads become detached and small	When micro-cracks are present due	
			to power handling inside the ceramic	
within specified power	This phenomenon is based on	detached load and the caramic.	bulk, the number of cycles can also	
handing capabilities)	re-crystalization of the solder when thermal stress is anniat	Fails open.	be limited. Short term name termenatures, as in	
	when thermal stress is applied. The number of cycles a normal		Short term peak-temperatures, as in an electronic temp ballast application.	
	FTC ceramic can have is depen-		an electronic lamp datast application, can handle a higher number of cycles	
	dert on the final temperature		(usually > 20000).	
	reached every cycle. A normal		A clamped PTC ceramic can handle	
	range of cycles can range from		a much higher number of cycles due	
	100 to \$000.		to a free contact movement during	
			heating up (number of cycles	
			> 300000). Cycline at low ambient temperature is	
			more severe because of the large dit-	
			ference between initial and final tem-	
			perstures.	
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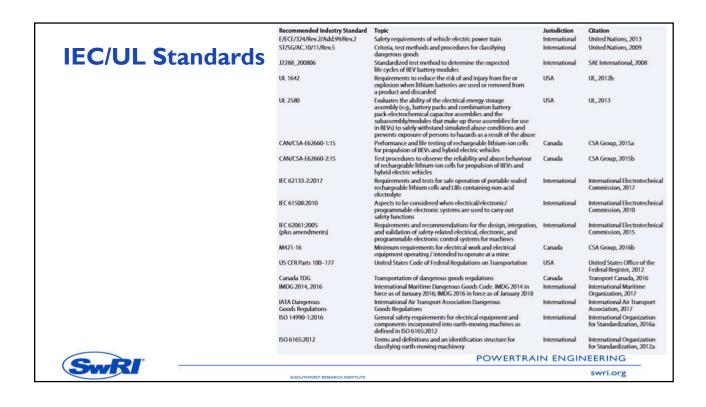
# **NFPA Cross Compatible EV Standards**

Document Title	
NFPA 1 Fire Code	
NFPA 30A Code for Motor Fuel Dispensing Facilities and Repair Garages NFPA 70 National Electrical Code (NEC); Article 220, Branch Circuit, Feeder and Service Calculations; Article 625, Electric Vehicle Charging Systems; Article 626, Electrified Truck Pa Spaces; and other req.	arking
NFPA 70B Electrical Equipment Maintenance	
NFPA 70E Electrical Safety in the Workplace	
NFPA 289 Fire Test for Individual Fuel Packages	
NFPA 450 Guide for Emergency Medical Services and Systems	
NFPA 471 Recommended Practice for Responding to Hazardous Materials Incidents	
NFPA 472 Competence of Responders to Hazardous Materials/Weapons of Mass Destruction Incidents	
NFPA 556 Guide on Methods for Evaluating Fire Hazard to Occupants of Passenger Road Vehicles	
NFPA 921 Fire and Explosion Investigation	
NFPA 1000 Fire Fighter Professional Qualifications Series (1000 – 1081)	
NFPA 1192 Recreational Vehicles	
NFPA 1500 Occupational Safety & Health Standards for Fire Fighters	
NFPA 1561 Emergency Services Incident Management System	
NFPA 1600 Disaster Planning and Emergency Preparedness	
NFPA 1670 Standard for Technical Rescue Incidents	
NFPA 1710 Organization and Deployment of Fire Suppression Operations, Emergency Medical Operations, and Special Operations to the Public by Career Fire Departments	
NFPA 1720 Organization and Deployment of Fire Suppression Operations, Emergency Medical Operations and Special Operations to the Public by Volunteer Fire Departments	
NFPA 1851 Selection, Care, and Maintenance of Protective Ensembles for Structural Fire Fighting and Proximity Fire Fighting	
NFPA 1971 Protective Ensembles for Structural Fire Fighting and Proximity Fire Fighting	
NFPA 1999 Protective Clothing for Emergency Medical Operations	
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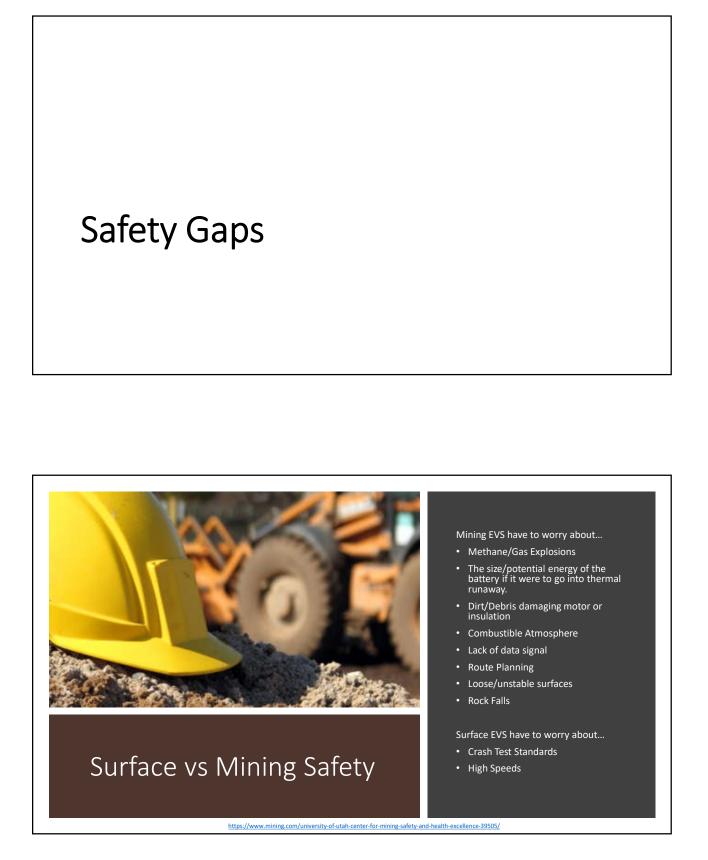
Type of Testing	Transportation	
Performance or Characterization	USABC PHEV Manual IEC 62660-1 IEC 61982 ISO 12405-1	
Cycle and Calendar Life	FreedomCAR (SAND 2005-3123) EUCAR* IEC 62660-2 IEC 61982 ISO 12405-1	
Abuse or Safety	SAE J2464 FreedomCAR (SAND 2005-3123) EUCAR* BATSO UN 38.3 UL 2271 UL 2580 ISO 12405-1	

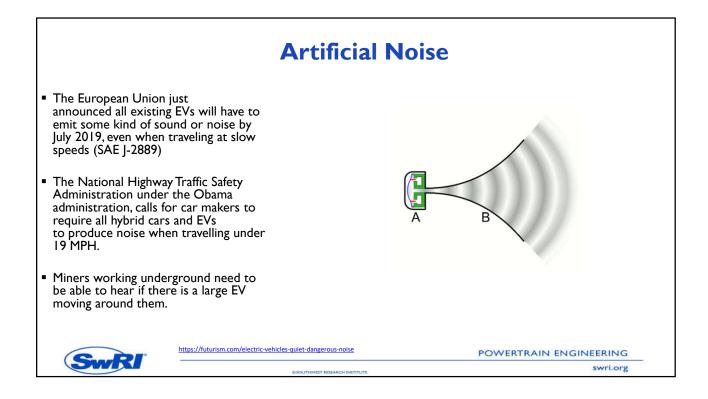
	Recommended Industry Standard	Торіс	Jurisdiction	Citation
	ISO 6405-1:2017	Standardizes symbols on operator controls and other displays on multiple types of earth-moving machines as defined in ISO 6165:2012	International	International Organization for Standardization, 2017a
<b>ISO Standards for EVs</b>	ISO 6405-2:2017	Standardizes symbols on operator controls and other displays on specific machines, equipment, and accessories as defined in ISO 6165:2012	International	International Organization for Standardization, 2017b
	ISO 6165:2012	Terms and definitions and identification structure to classify earth-moving machines	International	International Organization for Standardization, 2012a
	FMVSS 141	Minimum sound requirements for BEVs to warn persons that BEV is underway	USA	United States National Highway Traffic Safety Administration, 2013
	150 3450: 2011	Minimum performance requirements and test procedures for service, secondary, and parking brake systems of wheeled and high-speed, rubber- tracked earth moving machines	International	International Organization for Standardization, 2011a
	CAN/CSA-M424.3-M90 (R2016)	Minimum performance criteria for the service braking, secondary braking, and parking systems for rubber-tired, self-propelled underground mining machines	Canada	CSA Group, 2016a
	ISO 13849-1:2015	Safety requirements and guidance on design and integration of safety-related parts of control systems, including software	International	International Organization for Standardization, 2015b
	ISO 13849-2:2012	Procedures and conditions to validate—by analysis and testing—specified safety functions, the category achieved, and the performance level achieved by the safety-related parts of a control system designed in accordance with ISO 13849-12015	International	International Organization for Standardization, 2012b
Alanda Alan Alan A	ISO 14990-1:2016	General safety requirements for electrical equipment and components incorporated into earth-moving machines as defined in ISO 6165:2012	International	International Organization for Standardization, 2016a
	150 14990-2:2016	Safety requirements for electrical equipment and components incorporated in externally-powered (mains-connected or dedicated generators), electrically- driven earth moving machines	International	International Organization for Standardization, 2016b
	150 14990-3:2016	Safety requirements for electrical equipment and components incorporated in self-powered (utilizing on-board electric power sources) electrically-driven earth moving machines	International	International Organization for Standardization, 2016c
	ISO 13766:2006	Test methods and acceptance criteria for evaluating the electromagnetic compatibility of earth moving machines as defined in ISO 6165:2012.	International	International Organization for Standardization, 2006
	150 15998:2008	Performance criteria and tests for functional safety of safety-related machine-control systems using electronic components in earth moving machines and equipment as defined in ISO 6165:2012	International	International Organization for Standardization, 2008
	IEC 60068-2-6:2007	Standard procedure to determine the ability of components, equipment, and other articles to withstand specified severities of sinusoidal vibration	International	International Electrotechnic Commission, 2007
	IEC 60050-826:2004	Vocabulary related to electrical installations on residential, industrial, or commercial premises	International	International Electrotechnic Commission, 2004
	E/ECE/324/Rev.2/Add.99/Rev.2	Safety requirements of vehicle electric power train	International	United Nations, 2013
	ISO 13850:2015	Functional requirements and design principles for the emergency stop function on machinery, independent of the type of energy used	International	International Organization for Standardization, 2015
	IEC 60204-1:2016	General safety requirements of electrical, electronic, and programmable electronic equipment and systems to machines not portable by hand while working	International	International Electrotechnica Commission, 2006b
	UL 2231-1	Requirements to reduce the risk of electric shock to the user from accessible parts in grounded or isolated circuits (external to or on-board) for charging BEVs	USA	UL, 2012a
V	ISO 6469-3:2011	Requirements for electric propulsion systems and conductively connected auxiliary electric systems of electrically propelled road vehicles for the protection of persons inside and outside the vehicle against electric shock	International	International Organization for Standardization, 2011b
	ST/SG/AC.10/11/Rev.5	Criteria, test methods, and procedures for classifying dangerous goods	International	United Nations, 2009
	ST/SG/AC.10/1/Rev.17	Model regulations on the transport of dangerous goods	International	United Nations, 2011

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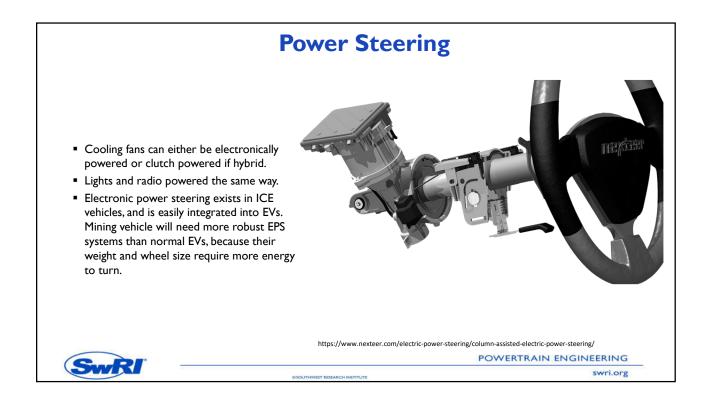


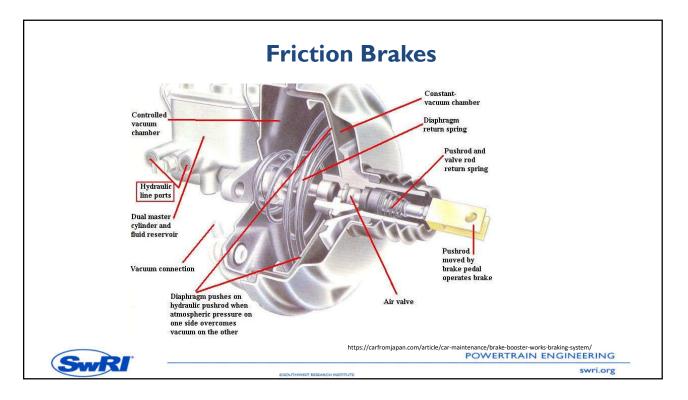
<b>Recommended Industry Standa</b>	d Toj	pic		Jurisdiction	Citation		
IEEE-519-2014	Est	Establishes goals for design of electrical systems that include both linear and nonlinear loads			Institute of Electrical and Electronics Engineers Standards Association, 2014		
IEC 61851-23:2014		Requirements for the control of communication			International Electrotechnical		
DIN SPEC 70121	between the DC charger and the BEV Specifies the DC-specific communication between the BEV and the electric vehicle supply equipment			Europe	Commission, 2014c Deutsches Institut für Normung e. V., 2014	stitut für	
Vehicle Haulage / water trucks	Fleet 8	Power (kW) 300	Loaded Weight (kg) 60,000	Battery (kWh) 400	Range for 15% Grade (km) 8-		
LHD machines	14	250	60,000	200	4		
Graders	1 4	100	20,000	200	12		
Drill and bolters Emulsion loaders	12	125	25,000	100	4		
Emulsion loaders Large utility vehicles	15	150	15,000	100	8	1	
Small utility vehicles	30	100	5,000	50	12		

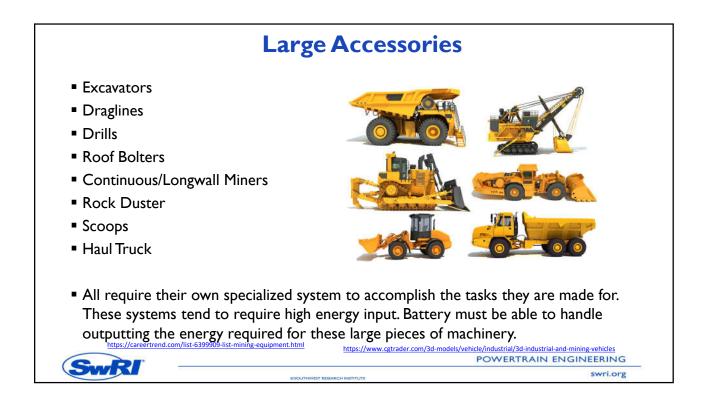


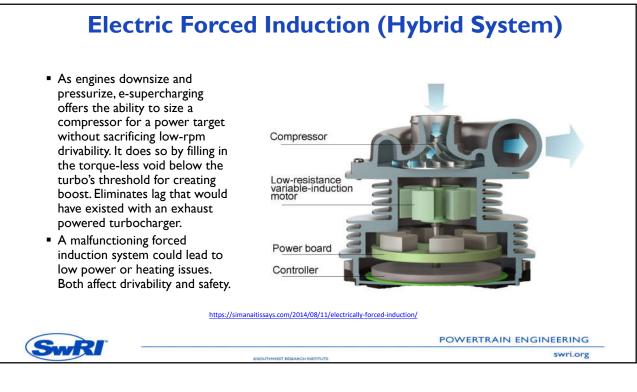












# **Cabin Temperature Control**

- EVs must use electrically driven compressors for AC, and electrical(resistive) heaters for heating (as opposed to belt driven AC and hot coolant in ICE). Resistive heaters work by increasing resistance with heat, which allows them to be quite efficient.
- Cabin temperature is important for miners, as they need to be able to focus on controlling their machinery, not trying to combat uncomfortable working conditions. A distracted operator, either from overheating or being too cold, poses as safety risk to people and equipment around them.





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#### **Effect of Air-Pressure on Lithium-ion**



In this study, an experimental test has been designed to determine the effect of external pressure on several electrical parameters such as GEIS, current, voltage, capacity variation and dynamic pressure generation for a pouch cell. Overall, GEIS measurement results indicate that the external static pressure couldn't change "ohmic contribution" but it could improve ion diffusion under pressure from 0.125MPa to 1MPa. Li-ion pouch cell can generate a dynamic pressure during charging and discharging around 50% SOC, this dynamic pressure generation coincides well with the capacity variation profiles. Moreover, the speed of dynamic pressure depends on current rate. Current rate does not influence the dynamic pressure with the ampere hours charged, however, it influences the cell voltage between 35% SOC and 65% SOC. To charge a cell, the high pressure generates with a high current rate. Based on these results, automotive industry could optimize the design of battery package.

 Pressure increases as the distance below ground increase. Charging a battery may be more efficient the further underground it is placed. However, there may be significant drawbacks that make deep bellow surface charging unviable.

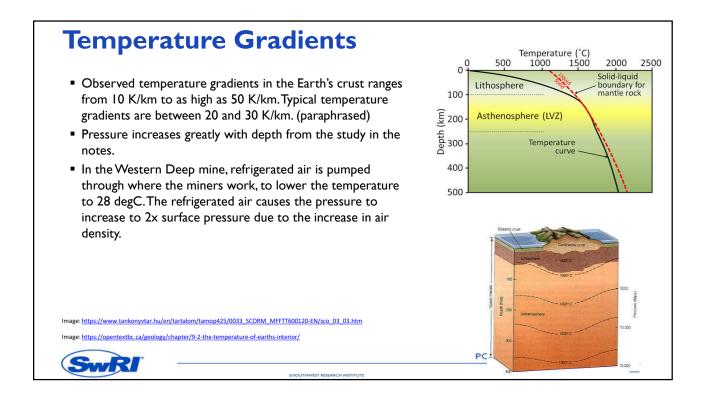
Characterization of external pressure effects on lithium-ion pouch cell, 2018, IEEE, Yuan Ci Zhang et. al

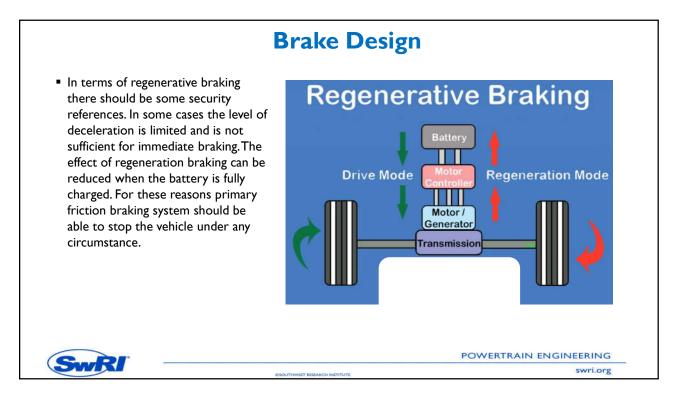


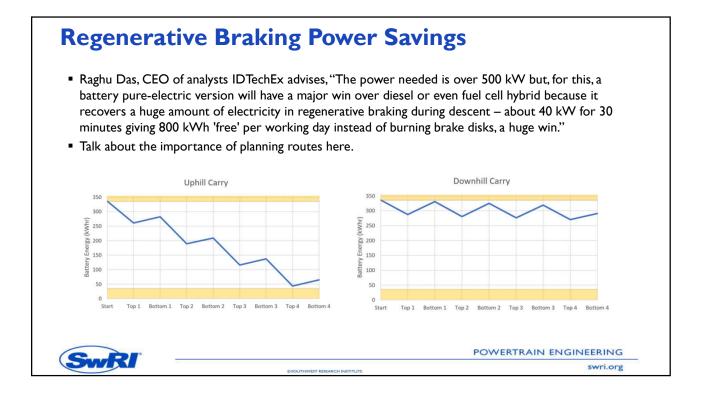
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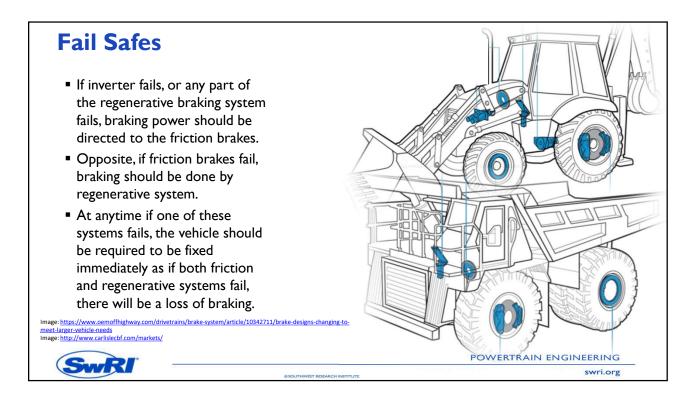


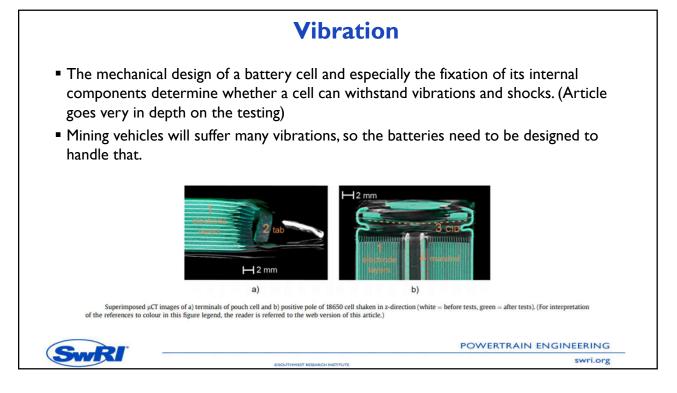
# **Regenerative Braking Issues**

- Regenerative braking can be a double-edged sword. A fully charged BEV that needs to
  make a long downhill journey may not be able to store the braking energy, and would
  rely on friction braking or braking resistors. It is best to avoid this situation
  altogether through careful planning, for example by positioning charging locations at
  the bottom of a ramp, or limiting the amount of charge taken on if a downhill trip is
  anticipated.
- While braking distance and feel should not be greatly changed when regenerative braking is inactive, operators must be aware of the switch to fully frictional brakes. If the friction brakes become too hot, there should be a system override to stop the vehicle, and let the brakes cool. An alternative solution to this is to have a cooling system activate on the friction brakes when they are in sole use. The cooling system should not be used if regenerative braking is active, as power absorption will be stunted.



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# **Holistic View**

# **Off Board Chargers**

- One possible remedy to these concerns is to use one OEM for the BEV drivetrain to standardize the entire mine. Experience has shown that dictating to OEMs the type of equipment and technology to use on board their BEVs stifles innovation, leads to complications, and yields a poorer product. This approach also increases risk because the mine completely depends on a single vendor
- As with the commercial BEV industry, the solution for mining BEVs may be to standardize the charging interface. Once the connector, voltage range, and communications between the charger and BEV are agreed upon, a BEV from one OEM could be connected to a charger from another OEM. An obvious consideration is to adopt a standard from the commercial BEV industry. However, the demands of a mining BEV differ from those of a passenger BEV. The entire charging arrangement needs to be rugged to withstand the harsh mining environment. The connectors, charger, voltages, charge rates, and communication methods need to be suitable for a mining BEV drivetrain and battery. If these issues can be addressed, then the mining industry would benefit from the research and development already invested by the commercial BEV industry. If not, then the development of a "mining only" interface may be the only solution.



### **Off Board Chargers Pros and Cons**

#### Pros

I. BEV size and weight are low because charging equipment is not on the BEV.

If practical, chargers can be located in cool and contaminant-free areas.
 High-capacity chargers are feasible because size and weight are not issues.

not issues. 4. Multiple BEVs can share one charger if connectors and communication protocols are compatible between BEVs. 5. Off-board charging is the charger standard in parallel industries such as public transport and port equipment.

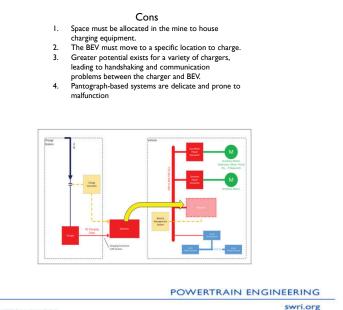
For proprietary charging interfaces, the responsibility for the entire system (i.e., drivetrain, batteries, and charger) lies with the OEM.

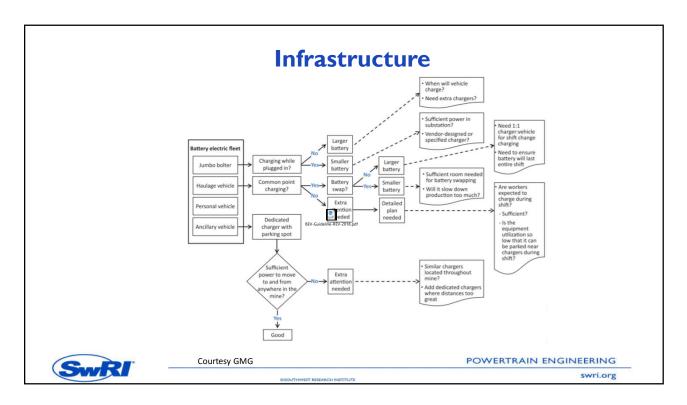
OEM. 7. BEV OEMs can focus on building high-quality mining BEVs, rather than developing or supplying chargers. Similarly, electrical equipment suppliers can develop rugged BEV chargers, without entering the BEV business. It is feasible for an OEM to build both chargers and BEV drivetrains, as long as the charging interface is standardized.

Those in charge of procuring mobile equipment are free to purchase any type of BEV from any OEM.
 The fixed plant department are free to purchase and install charging infrastructure regardless of the BEV OEM.

charging infrastructure regardless of the BEV OEM. 10. For equipment operators (instructed persons defined in International Electrotechnical Commission, 2004), a simple and consistent charging interface across the mine eliminates confusion and additional training. The type of BEV or location within the mine is irrelevant— simply plug in the BEV and initiate the charge. 11. From a risk perspective, the worry that "all eggs are in one basket" is greatly diminished. If one OEM has a technical issue, only one relationship is affected. If an OEM goes out of business, the mine does not have an entire fleet of unsupported equipment and infrastructure.

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# <text><list-item> Facilities • An eye wash system is vital in case any employee comes in contact with battery acid. The system should easily accessible as a close as possible to the work area without causing any adverse exposure. A best practice is to have fixed-pipe eye wash/showers system with a drain, as compared to relying on gravity-fed units. • Unobstructed distance: wash stations shall be located in an area that requires no more than 10 seconds to reach—thar's approximately 50 feet. If it is a high hazard, consult a medical professional to determine the appropriate distance for harsh asian caustics (high hazard-closer distance). Eye wash water ow: 3 gallons per minute for at least 15 minutes. Water temperature: Tepid, which is defined as 60°F to 100°F. Plumbed eye wash/shower inspection: The station should be a signage. Training:All employees who might be exposed to a chemical splash should be trained in the use of the equipment.





# Smoke Detectors in Battery Charging Stations

Smoke detectors are suitable for use in battery charging stations. Carbon monoxide monitors should only be used as fire detectors in battery charging stations in conjunction with a hydrogen detector, as hydrogen from the charging process can affect the CO sensor. If the CO sensor and hydrogen sensors both show increased readings then hydrogen pollution may be the cause of the apparent rise in CO, although a visual inspection will be necessary to confirm this. If only the CO reading increases it may indicate that a fire has broken out.





# **Safety Procedures When Charging Batteries**

Always secure a battery prior to moving or exchanging it. This normally is accomplished using manual stops and/or powered rollers on the battery changer to prevent the battery from falling off the changer. Chargers should be robustly mounted to a permanent fixing. Chargers should be connected with a suitable lockable isolator/breaker that is compatible with the charger. The charger should be installed to the manufacturer's recommendations. Full service access should be allowed for the trucks, batteries and chargers – taking note of all necessary access points.



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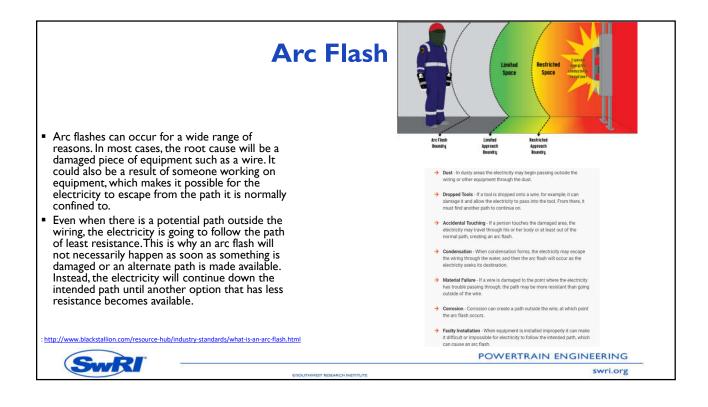
# **General Fire Precautions**

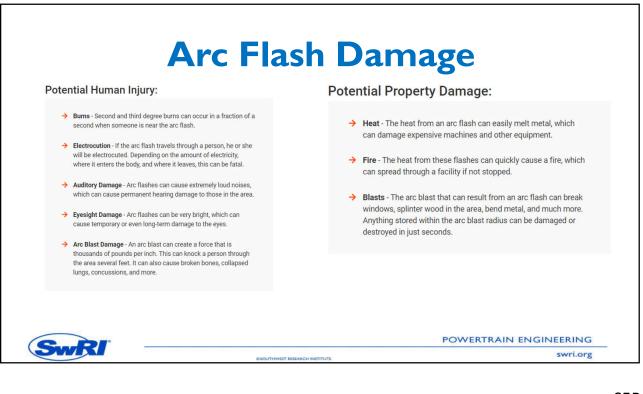
- The main stages of the fire and explosion assessment process are to:
- Identify the hazards the potential sources of ignition and materials that would cause a fire or explosion to spread
- ${\boldsymbol \cdot}$  Consider the precautions already in place for the prevention and mitigation of each fire and explosion hazard
- Evaluate the likelihood of a fire or explosion occurring due to a particular hazard
- ${\boldsymbol \cdot}$  Consider the consequences of a fire or explosion, and decide who might be harmed and how
- Determine what further measures are necessary to prevent, control or mitigate a fire or
  explosion
- Record significant findings; these should be included within the fire protection plan and the explosion protection plan required by regulation 4(2) of The Mines Miscellaneous Health and Safety Provisions Regulations 1995
- Review the risk assessment periodically, or when you think that a change in circumstances will significantly affect the risks to which people are exposed (e.g. moving from a non-gassy to a gassy seam).

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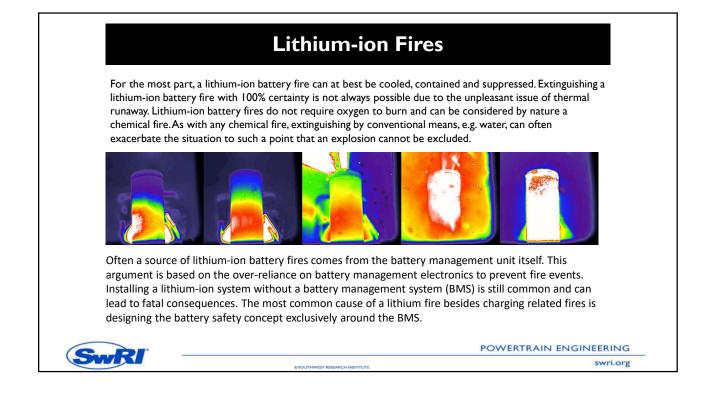
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### **Arc Safety** Whenever a machine needs to be worked on in any way, it should be completely de-energized. De-energizing a machine is more Ο than just turning it off.All machines should be shut down and physically disconnected from any power source. Once disconnected, a voltage check should also be done to ensure there is no latent energy that was stored up. DANGE Ideally a lockout tagout policy should be in place, which will put a physical lock on the electrical supply so that it cannot be accidentally plugged back in while someone is working on it. It should be very rare, but there are some cases when machines must be worked on while they are still energized. When this is the case, all employees working in the area should be required to wear proper personal protective equipment. DO NO The specific PPE that is worn should correspond to the maximum potential risk based on the amount of electricity going through OPER/ the machine. Having head to toe personal protective equipment can help to prevent serious injury or even fatalities should an arc flash occur while the machine is being worked on. Whenever possible, circuit breakers should be put in place on all machines. These breakers will guickly detect when there is a sudden surge in electricity being drawn and stop the flow immediately. Even with circuit breakers, an arc flash can occur, but it will EQUIPMENT LOCKED OUT BY only last a fraction of the time since the electrical current will be cut off. Even a very brief arc flash can be deadly, however, so circuit breakers should not be seen as a sufficient arc flash safety program. DEPT. XPECTED COMPLETION: https://www.creativesafetysupply.com/articles/arc-flash/ Image: https://www.jjkeller.com/shop/Product/Lockout-Tagout-Tag-Danger-Do-Not-Operate-Equipment POWERTRAIN ENGINEERING swri.org

### **Arc Flash Prevention** The first step in reducing the dangers of arc flash incidents is to perform an arc flash risk assessment. Safety managers who perform the examination (as outlined in NFPA 70E) can improve safety by: Collecting equipment data Identifying modes of operation Identifying bolted fault currents Identifying arc fault currents Identifying the devices' protective characteristics and duration of potential arc Documenting voltages and equipment classes Identifying working parameters Determining incident energy for equipment Identifying the required personal protective equipment (PPE) Identifying the arc flash boundary (1) Clay veins and related features have also been responsible for documented mine disasters. On November 9, 1888, 40 miners were killed by a gas explosion at Shaft No. 2, Frontenac, KS. It was noted in the investigation that the operation had "never seen gas in the mine except when cutting horsebacks or slips" [Humphrey 1960]. At the Hillside No. 1 Mine in Johnstown, PA, five miners were killed by a gas explosion on August 9, 1928. The explosion was caused when "a nonpermissible mining machine cut through a clay slip in a room face, releasing gas, which was ignited by an arc from the machine" [Humphrey 1960]. Only in-mine experience can alert the operator to experience of slaw using the experience of slaw using the experience of the machine of the ways of the experience of the e potential gas which was ignited by an arc from the machine [runnine (1960]. Only in-finite experience can aler the operator to potential gas emission problems due to the presence of clay veins. If excessive gas emissions are encountered when mining through these features, then underground mapping of clay veins is needed to predict their locations in future developments. Since clay veins frequently can extend hundreds of feet along a given trend [Chase and Ulery 1987], predicting a vein's occurrence in a developing section will allow the operator to anticipate and/or alleviate the potential problem. (2) POWERTRAIN ENGINEERING SwRI swri.org





# **Extinguishing Lithium-ion Fires Cont.**

Tesla publishes <u>emergency response guides</u> for all of its vehicles to help fire departments properly handle accidents involving the high-voltage cars. In the firefighting section of the Model S guide, the company mentions that—because burning lithium-ion batteries release "toxic vapors" including "sulfuric acid, oxides of carbon, nickel, lithium, copper and cobalt"—responders need to wear self contained breathing apparatuses. The section also mentions that, to extinguish a burning battery, responders have to "use large amounts of water to cool the battery." Companies that produce electric mining vehicles should also create similar content.

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Image: https://www.pinterest.com/pin/474003929506446066/

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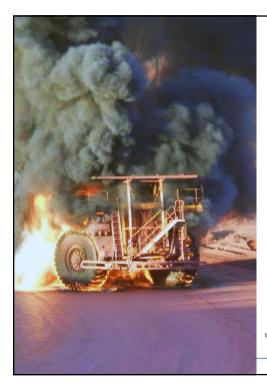
### **Disable the Vehicle and Powertrain**

- Determine the status of the vehicle by viewing the dash display, the position of the key in the ignition, and/or the power button to see if it has a lit indicator light. If the vehicle is "on", turn the key to the "off" position. Some new EDVs operate with a proximity key. If the proximity key is within range of the vehicle (usually less than 16 feet), the vehicle is powered "on" by a button on the dash. Turn the vehicle "off" by pressing this button. Then remove the key from the ignition and place it beyond the range of the vehicle (typically greater than 16 feet).
- In addition to the high voltage battery that powers an EDV motor, there is a conventional 12volt battery located somewhere on the vehicle. The 12-volt battery powers many of the vehicle accessories and is used to control high voltage contactors. Severing the 12-volt battery's ground cable will prevent the vehicle from powering up. Cutting the 12-volt battery in a vehicle that is "on", however, will not turn the vehicle "off", as power supplied by the DC/DC convertor may keep the contactor closed. After the vehicle has been powered down by the key/ignition button, firefighters should further disable the vehicle by severing the 12-volt battery's negative ground cable. The officer should refer to NFPA's Electric Vehicle Emergency Field Guide or other appropriate guides for vehicle specific information on the location of the 12-volt battery and fuses that can be pulled to disable the high voltage system.
- If firefighters are unable to gain access to the area housing the 12-volt battery or fuses, they may attempt to isolate the high voltage system by removing or switching off the high voltage main disconnect (or "high voltage service disconnect"). Firefighters will need a guide, such as NFPA's Electric Vehicle Emergency Field Guide, in order to determine the location of the high voltage main disconnect and identify the proper method for de-energizing the system. Firefighters may not be able to complete this step until after the fire is extinguished. Further detail on recommendations for high voltage system disabling can be found in SAE International Recommended Practice 1290.

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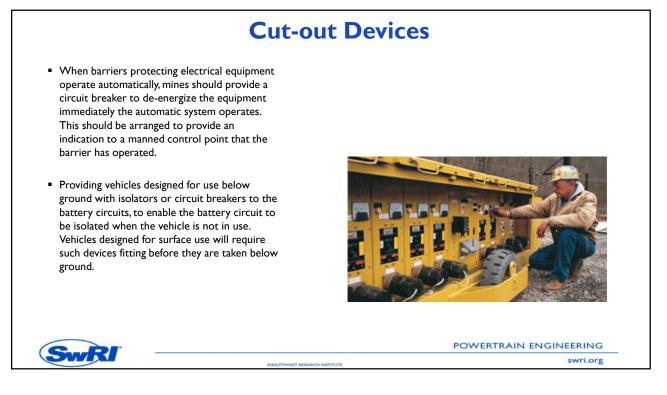
### **Extrication**

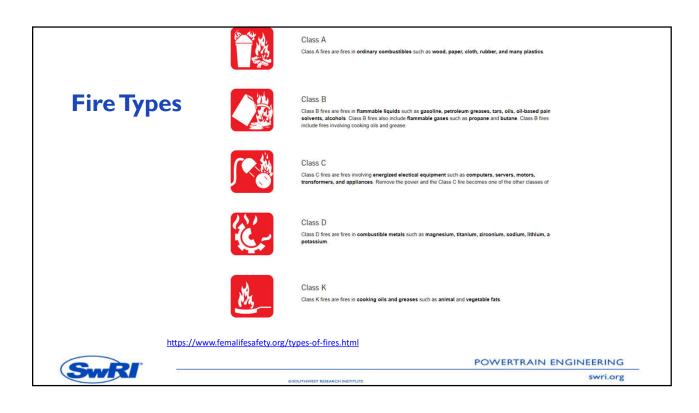
- A damaged high voltage battery may emit corrosive, toxic, and flammable fumes. If
  responders become aware of unusual odors and/or sense irritation of their eyes,
  nose, or throat, they should don PPE and SCBA. In addition, responders should
  use ventilation techniques to protect the occupants of the vehicle and prevent the
  build-up of flammable vapors in the trunk or passenger compartment.
- A charged attack line should be staged in close proximity to the vehicle during extrication. Responders should constantly monitor for indications that a damaged battery may be overheating, such as sparking, smoking or making bubbling sounds.
- Throughout stabilization and extrication, response personnel must avoid inadvertent contact with all high voltage cabling and high voltage components. Response personnel should never cut through any high voltage electrical component. Personnel performing the extrication should visually check for the presence of high voltage electrical cabling and components of the supplemental restraint system prior to initiating every cut or displacement (e.g. pry). The location and routing of high voltage components may prevent some advanced extrication techniques, such as trunk tunneling and gaining access through the underside or floor pan of the vehicle.

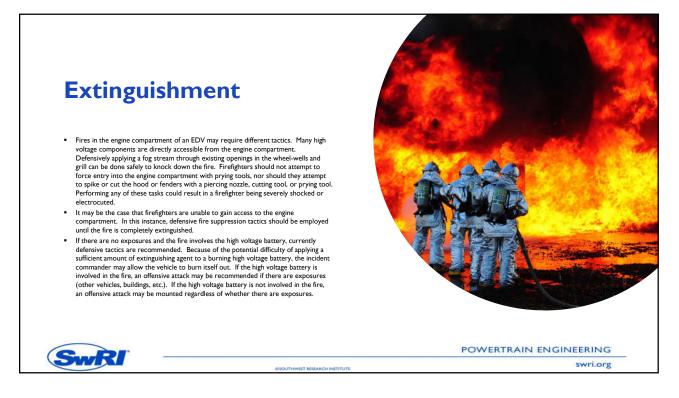
Image: https://firestormgroup.com.au/solutions/mining/

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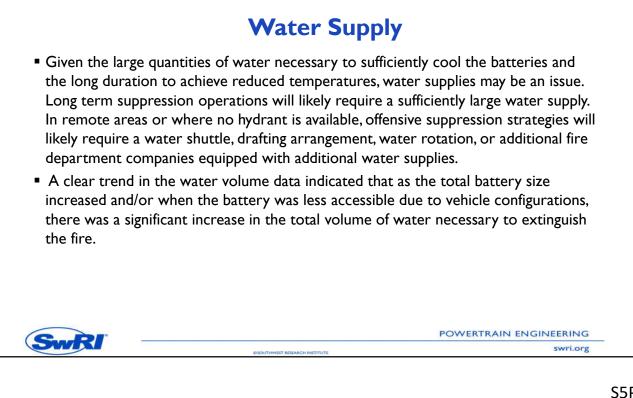
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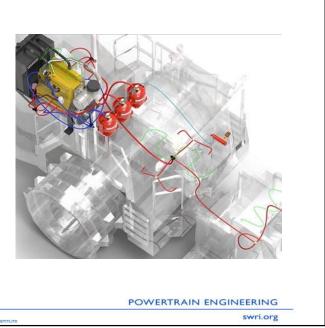


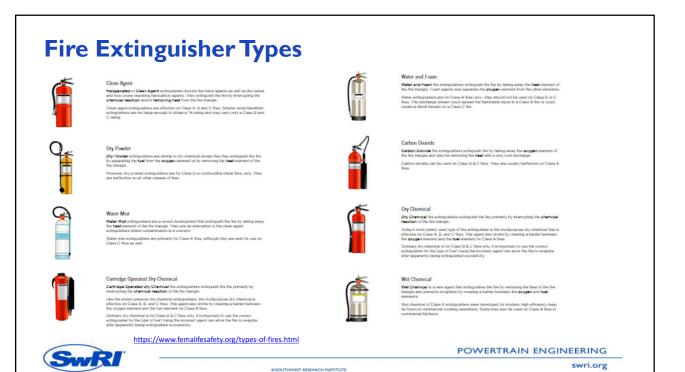
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### **On Board Fire Suppression**

Fire suppression system should be on board and placed in strategic areas around any driveline source of power. For EVs, this would be the electrical component system, as there are risks for fire all along it. For a hybrid, additional fire suppression should be placed around the engine and turbocharger. This system should only activate if the vehicle is truly on fire, and should act in such a way that it does not leave permanent damage from the extinguisher itself after the fire is extinguished.

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### **Fire Extinguishers**

- Mines should site fire extinguishers:
  - In conspicuous positions close to any machinery or equipment that gives rise to the fire risks. Below ground it should be sited on the intake side of the fire risk and in buildings it should be sited close to fresh air
  - On electrically powered mobile plant and equipment
  - At places where flammable materials are stored
  - In other locations indicated by the outcome of the fire risk assessment.
- Fire extinguishers should be provided near electric motors (other than those that are part of portable apparatus), transformers or switchgear (including electrical sub-stations, transformer houses, motor rooms and panel trains), workshops below ground, and battery charging and transfer stations
- Firefighters unanimously reported that access to the "hot spots" or "heat" was a significant barrier to extinguishing efforts.





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Image: https://www.omegasonics.com/uncategorized/ultrasonic-cleaners-meeting-nfpa-standards/

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### **Allowed burn**

Total water volumes were significantly greater in some tests than traditional ICE vehicle fires. In areas where a suitable water source is not present and there are no threats to life safety or to nearby structures, vehicles, or other combustibles, allowing the battery pack to burn to self-extinguishment may be a viable alternative to suppression. However, this may require extended periods of monitoring and observation for any reignitions. In the free burn test, the battery continued to visibly flame for approximately 90 minutes. Once it selfextinguished, it never reignited, although it did continue to off gas and was at elevated temperatures for hours afterwards.

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